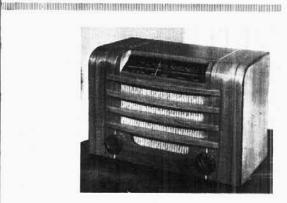
"TRADER" SERVICE SHEET

FERGUSC

S.W. and M.W. A.C. SUPERHET



STURDY chassis of new design, with rails permitting it to be stood on any side, and quick removal facilities, are commendable servicing features in the Ferguson 450, a four-valve (plus rectifier) two-band superhet designed for A.C. mains of 200-250 V. The two wavebands are S.W. (13.5-50m) and M.W.

Release date and original price: 1946; £14 14s, plus purchase tax £3 3s 3d.

CIRCUIT DESCRIPTION

Aerial input via coupling coils L1, L2 to single-tuned circuits L3 (S.W.), with L4 (M.W.), and C23, the bottom of the appropriate coil being connected via \$3 or \$4 to C4.

First valve (V1, Mullard metallised ECH35) is a triode-hexode operating as frequency changer with internal coupling. Oscillator anode coils L7 (S.W.) and L8 (M.W.) are tuned by C27. Parallel trimming by C26 (S.W.) and C25 (M.W.): series tracking by C7, via S7 (S.W.) and C24 (M.W.). On M.W., L7 and L8 are connected in series via \$8. Reaction via L5, L6.

Second valve (V2, Mullard metallised EF39) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned-primary, tuned-second-ary transformer couplings C28, L9, L10, C29 and C30, L11, L12, C31.

Intermediate frequency 470 kc/s.

Diode second detector is part of double diode triode valve (V3, Mullard metallised EBC33). Audio frequency component in rectified output is developed across R10 and passed via C15 and manual volume control R11 to C.G. of triode section. I.F. filtering by C11, R9, C12 and C16.

Second diode of V3, fed from V2 anode via C14, provides D.C. potentials which are developed across R14, R15 and fed back through decoupling circuits as G.B. to F.C. and I.F. valves, giving automatic volume control. Delay voltage, together with G.B. for triode section, is obtained from drop along R13 in cathode lead to chassis.

Resistance-capacitance coupling by R12, C17 and R16 between V3 triode and pentode output valve (V4, Mullard EL33). Negative feed-back from potential divider

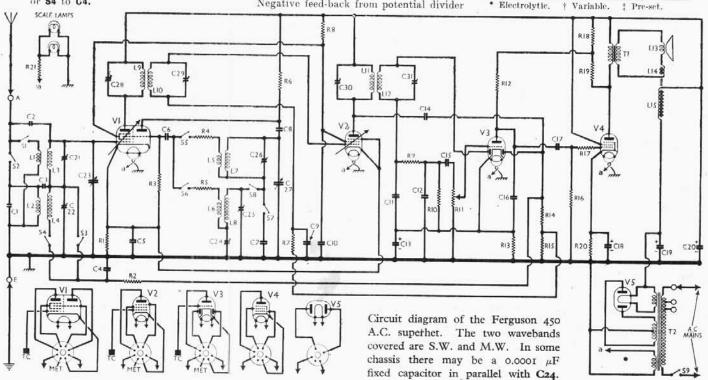
R18, R19 across T1 primary to V3 triode anode circuit, R18 being common to both circuits.

H.T. current is supplied by full-wave rectifying valve (V5, Mullard AZ31) Smoothing by speaker field L15 and dry electrolytic capacitors C19, C20.

COMPONENTS AND VALUES

CAPACITORS	Values (μF)
Aerial M.W. shunt	0-00002 0-000002 0-000005 0-1 0-1 0-0001 0-0001 0-0001 0-0001 0-0001 0-0001 0-00003 0-00003 0-00003 0-00008 0-00018 0-00018 0-00018

* Electrolytic.



Supplement to The Wireless &

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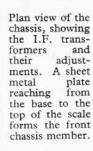
	Values (ohms)	
RI	V1, V2 fixed G.B. resistor	150
R2	VI hex. C.G. decoupling	680,000
R3	V1 osc. C.G. resistor	56,000
R4	Osc. S.W. reaction damping	50
R5	Osc. M.W. reaction damping	2,700
R6	V1 osc. anode H.T. feed	22,000
R7	V2 C.G. decoupling	680,000
R8	V1, V2 S.G.'s H.T. feed	27,000
R9	V3 signal diode load	56,000
R10	V3 signal diode load	680,000
R11	Manual volume control	2,000,000
R12	V3 triode anode load	56,000
R13	V3 G.B. resistor; A.V.C.	
	delay	1,500
R14.	V3 A.V.C. diode load re- f	680,000
R15	sistors \	680,000
R16	V4 C.G. resistor	680,000
R17	V4 grid stopper	4,700
R18	Negative feed-back resis- f	4,700
R19	} tors {	100,000
R20	V4 G.B. resistor	200
R21	Scale lamp ballast	

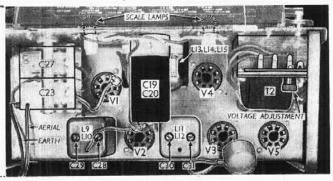
	Approx. Values (ohms)	
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 L14 L15	Aerial S.W. coupling coil Aerial M.W. coupling coil Aerial S.W. tuning coil Osc. S.W. reaction coil Osc. M.W. reaction coil Osc. M.W. tuning coil Osc. M.W. tuning coil Ist I.F. trans. { Pri Sec Pri Speaker speech coil Hum neutralising coil Speaker field coil Pri	1·4 30·0 Very low 3·0 0·15 1·0 Very low 2·0 8·5 8·5 8·5 8·5 8·5 3·0 0·1 1,200·0 450·0
T1 T2	Speaker input trans. { Pri. Sec. Pri., total Heater sec.	0·4 31·0 0·2
S1-S8	trans. Rect. heat sec H.T. sec., total Waveband switches	0·2 550·0
89	Mains switch, ganged R11	

GENERAL NOTES

Switches .- S1-S8 are the waveband switches, ganged in a two-position rotary unit, indicated in our under-chassis view and shown in detail in the diagram in col. 2, where it is drawn as seen from the rear of an inverted chassis. All the odd-numbered switches S1, S3, S5, S7 close on S.W. only, and all the even ones close on M.W. only.

S9 is the Q.M.B. mains switch, ganged with the volume control R11.





Scale Lamps.-These are two Osram M.E.S. types, with small spherical bulbs, rated at 6.5 V, 0.5 A. R21 is in series with them.

Speaker .- No provision is External made for this, but one of low impedance (about 5 Ω) could be connected to the

capacitors C19, C20.—These are two 16 μF dry electrolytics in a single cardboard tubular container mounted horizon-

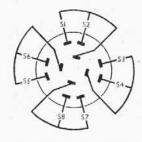


Diagram of wavethe band switch unit, as seen from the rear of an inverted chassis.

tally through a hole in the vertical front chassis member. They are rated at 450 V D.C. working. The red and plain tags are the positive connections, and the black tag is the common negative connection.

Chassis Divergencies.-R21 was not shown on the makers' original diagram, but it should be present to reduce the strain on the scale lamps. A 0.0001 µF capacitor shown in the makers' diagram in parallel with C24 was not present in our sample, but it is added in cases where the capacitance of C24 is required to be increased beyond its maximum. In some cases, also, R9 may be $50,000 \Omega$.

CIRCUIT ALIGNMENT

I.F. Stages .- Switch set to M.W., and turn the gang and volume control to maximum. Connect signal generator to control grid (top cap) of V1, via a 0.1 μF capacitor, and chassis, removing normal cap connector and connecting a 500,000 Ω resistor between it and the valve cap. Feed in a 470 kc/s (638.3 m) signal, and adjust C28, C29, C30 and C31 for maximum output. Replace top cap connector.

R.F. and Oscillator Stages.—With the

gang at maximum, pointer should be in line with the scale end markers. Transfer signal generator leads to A and E leads via a suitable dummy aerial. This may be a 0.0002 µF capacitor for M.W., but it is very important that it should be a 400 Ω resistor for S.W.

M.W .- Switch set to M.W., tune to 214 m on scale, feed in a 214 m (1,400 kc/s) signal, and adjust C25, then C22 for maximum output. Feed in a 500 m (600 kc/s) signal, tune it in, and adjust C24

for maximum output, while rocking the gang. Recheck at 214 m.

S.W.—Switch set to S.W., tune to 20 Mc/s on scale, feed in a 20 Mc/s (15 m) signal, and adjust C26 for maximum output, taking care to select the peak involving the lesser trimmer capacity if two are found. Then adjust C21 for maximum output, while rocking the gang for optimum results. Check at 6 Me/s (50 m).

DISMANTLING THE SET

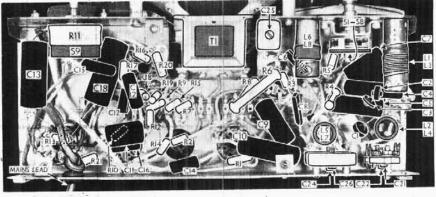
Pull off the three control knobs, taking care not to lose the springs, and remove the three screws (with washers) holding chassis to bottom of cabinet.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those quoted by the makers, who give the unsmoothed H.T. voltage as 320 V, smoothed H.T. as 250 V, total H.T. current as 53 mA, and total mains current as 200 mA, A.C. Readings were taken when the receiver was working at its longest wavelength on the M.W. hand, with volume control at maximum and no signal input. Voltages were measured on the 480 V range of a Model 40 Avometer, chassis being the negative connection.

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Current (mA)
V1 ECH35	250 Osc 140	$\left\{ \begin{array}{c} 2\cdot 1 \\ \text{illator} \\ 4\cdot 1 \end{array} \right\}$	145	1.6
V2 EF39 V3 EBC33	250 120	3.8	140	2.2
V4 EL33 V5 AZ31	240 315†	31.0	250	2.4

† Each anode, A.C.



Under-chassis view, showing the R.F. and oscillator coils and the position of the waveband switch unit.