FERRANTI 255, 355 and 455

a.m.-f.m. receivers

ODEL 255 is a 5+1 valve table radio for a.c. mains, covering m.w., l.w. and f.m. bands. Model 355 is a radiogram version using a Collaro RC54 or Garrard RC110 autochange unit and output via a 10in. dia. speaker. Model 455 is a bureau-type autochange radiogram with output via twin 8in. speakers and using a modified audio section.

CIRCUIT DETAILS

A.M. Reception

The signal input is conveyed via front and rear wafers of the wave-change switch section 4, to the grid of V2A operating as mixer. Signals are tuned by L11, C21 (m.w.) or L12, C22, C23 (l.w.) with C25, C26, main tuning gang. V2B is a conventional tuned grid local oscillator; L17/L18 m.w. transformer, L19/L20 l.w. transformer, trimmed by C38 and C39 respectively.

The i.f. signal (470 kc/s) is fed via L13/L14 to the i.f. amplifier V3. The a.m. and f.m. transformers are connected in series; when set is switched to a.m., the reactance at 470 kc/s of the f.m. transformer primary L15 is an effective short circuit; when switched to f.m., the reactance at 10.7 Mc/s of C31 is so low

as to represent an effective short circuit. Harmonics of the local oscillator (a.m.) appear around 10.7 Mc/s and to prevent absorption and loss of gain L16 is short circuited when set is switched to a.m. bands.

The amplified i.f. signal is then fed to a diode of V4, via L21/L22, and is demodulated, the a.f. voltage appearing across the load R18/R19 being fed via section 1 (rear) of the wave-change switch to the volume control R25, thence to the triode section of V4. The d.c. component present in the output of the demodulator is fed back, via filters, to V2A and V3 as a.g.c. bias.

The amplified a.f. signal is then fed to V5, a conventional power output valve with negative feedback and a manual tone control (R34) in the coupling network. Power is provided by means of a full-wave mains rectification system of conventional a.c. design.

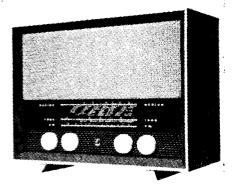
F.M. Reception

Signal input is fed via r.f. transformer L1/L2 to the cathode of V1A, operating as a grounded grid r.f. amplifier, the output of which is fed to the oscillator feedback coil L4 via L3 and C4. The tapped coil L4, with C7 and the V1B grid-cathode capacitance, form a simple bridge network.

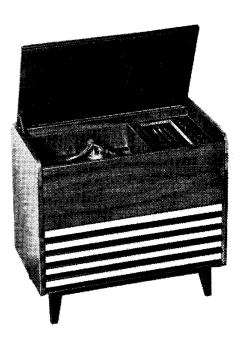
C7 is adjusted to balance the bridge at the mid-oscillator frequency so that oscillator voltage at L4 tap is reduced to a minimum and so reduces oscillator radiation via C4 to the r.f. and aerial circuits

I.f. signals at 10.7 Mc/s are developed across L6. The decoupling resistor R4 is only partially bypassed by C3 so that a portion of the i.f. signal appears at the junction of R4 and C3. This signal is coupled back via L3-C4-L4 into the oscillator grid, it is amplified and appears across L6 to reinforce the original signal. Thus, V1A functions both as mixer-oscillator and regenerative i.f. amplifier.

On f.m. operation, V2A functions as an i.f. amplifier, the output of which is coupled via L15/L16 to the 2nd i.f. amplifier V3 which is driven into grid



Model 255



Model 355

RELEASE DATES AND PRICES Model 255T: Sept., 1956; 25 gns. Model 355RG: Sept., 1956 59 gns. Model 455RG: Sept., 1956, 79 gns. All prices tax paid.

current, resulting in amplitude limiting and producing a negative bias which tends to maintain a constant output. A d.c. voltage which varies with average carrier level is derived from the ratio detector and applied to G3 of V3 to assist the a.g.c. action.

Two diodes of V4 are arranged in a ratio detector circuit, fed from the discriminator transformer L23/L24. The demodulated output is fed via the tertiary winding on the discriminator transformer, de-emphasis and a.f. load components and the switch to the volume control and thence to the audio stages as for a.m. operation.

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SERVICE SNAPS

FERRANTI 255, 355 and 455

Valves: Models 255 and 355— ECC85, ECH81, EF85, EABC80, EL84, EZ80. Model 455—ECC85, ECH81, EF85, EABC80, ECC82, two EL84, GZ32.

Dial Lamps: Models 255 and 355
—two 6.3V 0.2A. M.E.S.
Model 455—three 6.5V 0.3A.

Intermediate Frequencies: A.m.—470 kc/s. F.m.—10.7 Mc/s.

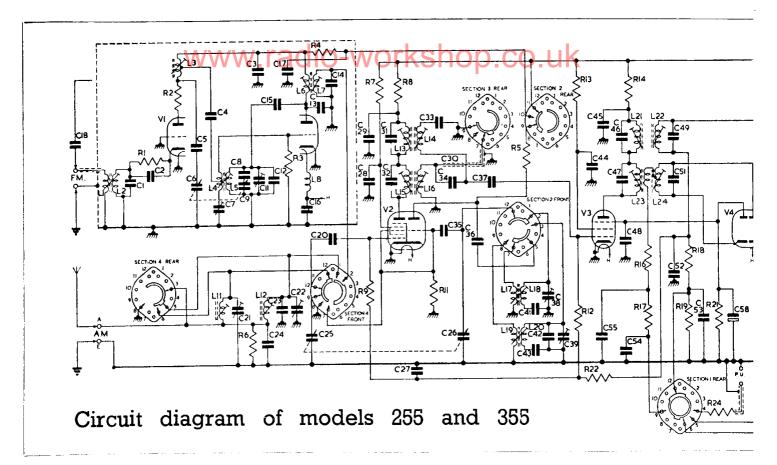
470 kc/s. F.m.—10.7 Mc/s. Volume Control: $1M\Omega$ log. (Models 255 and 355), $1M\Omega$ log, tapped at 200kΩ (Model 455).

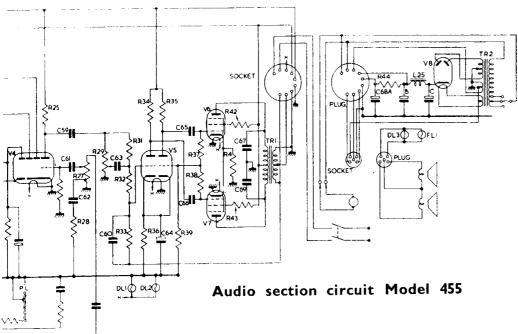
Tone Control: $500k\Omega$ inv. log with d.p. switch (Models 255 and 355), or $1M\Omega$ lin. with d.p. switch (Model 455).

Electrolytics: $5\mu F$, 50V; $25\mu F$, 25V; $32 - 32\mu F$, 350V (Models 255 and 355) or $24 + 24 + 16\mu F$, 350V (Model 455).

Wavebands: 190-570m (m.w.), 1,000-2,000m (l.w.) and 87.5-100 Mc/s (f.m.).

Mains input: 200-250V a.c. only.





Model 455

This bureaugram version is exactly the same as Models 255 and 355 up to the triode section of the EABC80, V4. The output from V4 is fed to a double-triode phase splitting stage V5 (ECC82) which drives a pair of EL84's in push-pull. The power supply circuit is also slightly different as shown above. The high h.t. line feeds, in addition to the output valve screens, the V3 and V2A anodes. The lower h.t line feeds the remainder of the anodes and screens of the pre-detector stages.

New component values are shown alongside.

| | An | Anode | | Screen | | |
|-----|----------|-------|-----|--------|-----|--|
| | V | mA | V | mA | V | |
| VIA | 160 | 6 | | _ | 1.5 | |
| VIB | 160 | 6 | _ | | | |
| V2A | 225 | 2.7 | 70 | 5 | _ | |
| V2B | 85 | 4.5 | | _ | | |
| V3 | 220 | 7 | 53 | 1.8 | | |
| V4* | 70 | 0.5 | | | | |
| V5 | 265 | 40 | 230 | 4.5 | 6.3 | |
| V6 | <u> </u> | | i — | | 280 | |

*Triode section
On f.m. operation voltages are slight! On f.m. operation voltages are slightl lower than figures quoted above, anod and screen currents slightly higher. O f.m., V2B anode is disconnected from h.t., o gram V1 and V2B anodes are disconnected Readings taken with Model 8 Avomete Smoothed h.t. at low end of R31—230 Total h.t. current at V6 cathode 65m. (a.m.) or 70mA (f.m.).

| | Resistors | R38 | 390kΩ | | C62 | 0.00 |
|-----|-----------|-------|-------------------|---|------|-----------|
| R25 | 100kΩ | R39 | 470kΩ | i | C63 | 30 |
| R27 | 1MΩ* | R41 | 130Ω, 1W | 1 | C64 | 25μF, |
| R28 | 100kΩ | R42 | 100Ω | | C65 |).0 |
| R29 | 1ΜΩ | R43 | 100Ω | | C66 | 0.0 |
| R31 | 470kΩ | R44 | $2.2k\Omega$, 1W | | C67 | 0.00 |
| R32 | 100kΩ | *Tapr | | i | | 400√ |
| R33 | 330kΩ | | | 1 | C68A | 24 u.F. 1 |
| R34 | 100kΩ | ! | | İ | C68B | 24 u.F. (|
| R35 | 100kΩ | (| apacitors | ! | C68C | 16µF, 1 |
| R36 | 1.5kΩ | C59 | 0.01 uF | | C69 | 0.00 |
| R37 | 390kΩ | C61 | 0.01µF | | | 400℃ |
| | | | | | | |

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| Capacitors C1 C2 C1 C3 C3 C4 C50PF, 5% C4 C50PF, 5% C5 C5 C5PF, 5% C6 C7 C7 C8 C9 C9 C11 C9 C11 C12 C14 C20PF, 5% C14 C20PF, 5% C15 C15 C16 C10 C16 C17 C17 C18 C19 C19 C20 C30 C41 C40 C50 C51 C50 |
|---|
| C39 3-40pF |
| |

| | 0 1 0 |
|----------|---|
| wkg | 430pF, 1% 150pF, 5% 200pF, 2% 0.005μF 0.005μF 100pF, 5% 33pF, 2% 0.002μF 300pF, 5% 40pF 100pF 0.001μF 300pF 0.005μF 0.01μF 300pF 0.005μF 0.005μF 0.005μF 0.005μF 500V 0.05μF 50V 200pF 25μF, 25V 32μF 32μF 32μF 32μF 32μF 3005μF, 300V unless other-stated. |
| R1 | Resistors 220Ω |
| R2 | 10Ω |
| R3 | 1MΩ, {W |
| R4 R5 | 4.7kΩ, IW 33kΩ, IW |
| | 22.114, 111 |

| R6 | 3.3kΩ |
|-----------|-----------------|
| R7 | |
| | 33kΩ, 1W |
| R8 | 2.2kΩ |
| R9 | IMΩ |
| RII | |
| KII. | 47kΩ |
| R12 | 220kΩ |
| R13 | 100kΩ, ½W |
| R14 | 2.2kΩ |
| R16 | 47Ω |
| R17 | |
| | 39kΩ |
| R18 | 220kΩ |
| R19 | 470kΩ |
| R21 | 27kΩ |
| R22 | IMΩ |
| N.22 | |
| R23 | 47kΩ |
| R24 | 220kΩ |
| R25 | 1MΩ |
| R26 | 470kΩ |
| R27 | |
| R27 | 100kΩ |
| R28 | 220kΩ |
| R29 | 10MΩ |
| R31 | 1.8kΩ, 4W |
| R32 | 220kΩ |
| R33 | |
| | 100kΩ |
| R34 | 500kΩ |
| R35 | 150Ω, ½W |
| R36 | 470kΩ |
| | stors ‡W un- |
| lage oak | stors Tw un- |
| iess otne | erwise stated. |
| | |
| | Valves |
| VI | ECC85 |
| 1/2 | ECITO |

| | Valves |
|----|--------|
| VI | ECC85 |
| V2 | ECH81 |
| V3 | EF85 |
| V4 | EABC80 |
| V5 | EL84 |
| V6 | EZ80 |

PRODUCTION MODS

F.M. Sensitivity

In later models, C3 is 390pF and C5 is 50pF, these changes giving increased sensitivity on f.m. operation. In introducing these changes to earlier receivers, C3 leads must be kept very short and the earth connection made to the end of the capacitor marked with a black

Re-trimming of the r.f. circuits will be necessary to correct calibration. In a few receivers, low gain when using the internal aerial may be due to short-circuit by the aerial strip of C18 due to the positioning of the tag panel on which C18 is mounted.

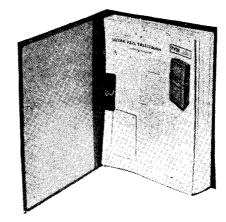
Crackles

In later models, the dial lamp circuit is earthed via a lead from the dial lamps to a chassis earth tag. Where crackles are experienced, due to poor contact between lamp holders and dial assembly, the lead should be added.

Record Changer Noise

Later models using the RC54 record changer are fitted with a cushion spring on the striker feed lever to prevent the rhythmical tapping noise caused by the auto trip lever. A spring and fitting instruction can be obtained from the Ferranti service department for earlier grams in which the noise is apparent.

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When carrying out full realignment, the a.m. circuits should be trimmed before the f.m. circuits, as follows:

I.F. Alignment

Inject 470 kc/s into pin 2 of V2 via 0.1 µF capacitor and with receiver tuned to 2,000m (maximum l.w.) tune L22, L21, L14 and L13 for maximum gain, taking first peak as core is screwed in.

R.F. Alignment

Tune receiver to 500m, inject signal of 600 kc/s to aerial socket via standard dummy aerial and adjust L17/L18 and ring on L11 for maximum output. Tune receiver to 200m, inject 1,500 kc/s and trim C38 and C21 for maximum output. Repeat.

Tune receiver to 1,800m, inject 166.6 kc/s and trim L19/L20 and ring on L12 for maximum output. Tune receiver to 1,128m, inject 266 kc/s and trim C39 and C22 for maximum.

Repeat.

Note that aerial rod rings should be resealed with wax after alignment.

F.M. ALIGNMENT

I.F. Circuits

Method 1: Using a.m. signal generator connected to f.m. aerial sockets, 10V d.c. high resistance meter across R21 for i.f. alignment and a 100V a.c. meter across TR1 primary or a 3V a.c. meter across speaker for discriminator (L24) alignment. Signal input to be kept about the level to give about 5V across R21 or 10-20V across TR1 or 1.2V across speaker.

Unscrew core of L24 to nearly fully out. Inject 10.7 Mc/s and trim L23, L16,

L15, L7 and L6 for maximum volts across R21. Inject 10.7 Mc/s, modulated 30 per cent, and trim L24 to *minimum* dip between two peaks.

To check bandwidth, detune signal generator in equal steps of, say, 50 kc/s up to 200 kc/s above and below the i.f., recording output voltage across R21 at each step and graphing results. Response

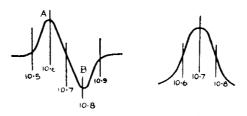


Fig. I (Left): Discriminator "S" response curve. Fig. 2 (right): Pre-detector i.f. response curve.

shape must be substantially symetrical and voltage at 10.6 and 10.8 Mc/s should be approximately 6dB below voltage at 10.7 Mc/s.

Method 2: Using f.m. signal generator, deviation ± 75 kc/s, with 1 kc/s tone modulation.

Unscrew L24 core nearly fully out and trim all i.f. circuits as before. Then tune L24 for *maximum* audio output obtainable with minimum distortion. Slight mis-tuning can be detected on either side of the correct tuning point as sharp increase in distortion.

An oscilloscope can be connected across audio output to indicate correct tuning point for L24, the core of which

should lie centrally between the two points where distortion occurs as indicated by marked flattening on peaks.

Method 3: Using f.m. oscillator (±300 kc/s deviation), the output of which is fed to receiver aerial sockets, and an oscilloscope whose sweep waveform (about 150V d.a.p. at 50 c/s) is used to modulate the signal generator, the amplifier being connected to volume control for discriminator response or to V3 anode via suitable probe for i.f. response.

An a.m. signal generator is also required, in parallel with f.m. oscillator, to provide calibration markers, unless this facility is available in f.m. oscillator.

Tune receiver to about 94 Mc/s and signal generator to 10.7 Mc/s, adjusting attenuator so that waveform trace on 'scope is about 0.2V d.a.p. (Fig. 1). Section of trace between A and B should be linear and symetrically centred on 10.7 Mc/s; non-linearity is affected by L24, centring by L23, the adjustments being somewhat interdependent. Slight readjustment of i.f. cores may be necessary for optimum results.

If desired, the pre-detection i.f. response can be independently examined by transfering c.r.o. amplifier input connections to V3 anode via diode probe. Response is shown in Fig. 2.

R.F. Circuits

Inject 90 Mc/s signal into f.m. aerial socket, using either a c.w. signal with a 10V d.c. meter across R21 or a ± 25 kc/s f.m. signal with output indicator across TR1 or speaker. Adjust L4/L5 for maximum gain.

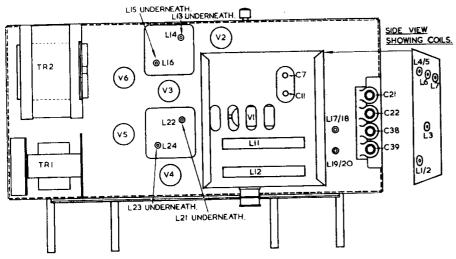
Retune receiver and signal input to 98 Mc/s and trim C11. Repeat 90 and 98 Mc/s trimming. Then retune to 94 Mc/s and trim L3.

INCORRECT ALIGNMENT

If receiver is correctly trimmed, a marked dip in interference will occur when station is correctly tuned in. Poor noise rejection or distortion indicates incorrect setting of L23 and L24, causing poor linearity and/or assymmetry of response characteristics.

OSCILLATOR RADIATION

After extensive repairs, adjustment may be necessary to reduce oscillator radiation. Remove screening box and connect valve voltmeter (maximum f.s.d. 1V with short probe leads) between junction of L3/C4 and chassis. Tune receiver to 94 Mc/s and adjust C7 for minimum indication first minimum as core is screwed in.



Sketch of receiver chassis from above, with side view of r.f. unit, showing location of trimming positions.