"TRADER" SERVICE SHEET

ITTED with a quick-release device for rapid removal of the chassis, the Kolster-Brandes HR10 receiver is a 4-valve (plus rectifier) 3-band superhet designed to operate from A.C. mains only of 200-250 V, 50-100 c/s, via an auto-transformer. The chassis is "live" to the mains. A three-core mains lead permits earthing of the external speaker circuit where a 3-pin wiring system is employed. The waveband ranges are 16.3-51 m, 187-570 m and 880-2,100 m.

The HG30 is an autoradiogram employing a Garrard 3-speed record-changer. The chassis in it is a modified version of the HR10, the main differences being in the audio frequency circuit, but it is also fitted with a double-wound mains transformer, and the chassis can be earthed

Release date and original prices: August 1952 (both models); HR10, £16 os 5d; HG30, £52 198. Purchase tax

CIRCUIT DESCRIPTION

Aerial input via L1 (S.W.) and "bottom'' capacitative coupler C4 (M.W. and L.W.) to single tuned circuits L2, C28 (S.W.), L3, C28 (M.W.) and L4, C28

adib Workshop.co.uk KOLSTER - BRANDES

and HG30 Autoradiogram

(L.W.), which precede heptode valve (V1, Brimar 6BE6) operating as frequency changer with electron coupling.

In the table model the A and E sockets are isolated by C1 and C2 from the chassis, which is "live" to the mains. R1 prevents the build-up of static charges on the aerial, and R2 provides a shunt path for modulation hum components. In the gram model a double-wound mains transformer is used, isolating the chassis from the mains input and making R1, C2 and C3 no longer necessary, and these components are omitted as indicated in the circuit diagram.

Oscillator grid coils L5 (S.W.), L6 (M.W.) and L7 (L.W.) are tuned by C29. Parallel trimming by C30 (S.W.), C31 (M.W.) and C11 (L.W.); series tracking by C9 (M.W.) and C10 (L.W.) in the high potential ends of the circuits. Reaction coupling from cathode by coils L8 (S.W.), L9 (M.W.) and by a tap on L7

(L.W.) Oscillator stabilization by R5. Second valve (V2, Brimar 6BA6) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C6, L10, L11, C7 and C16, L12, L13, C17.

Intermediate frequency 422 kc/s.

Diode signal detector is part of double diode triode valve (V3, Brimar 6AT6).

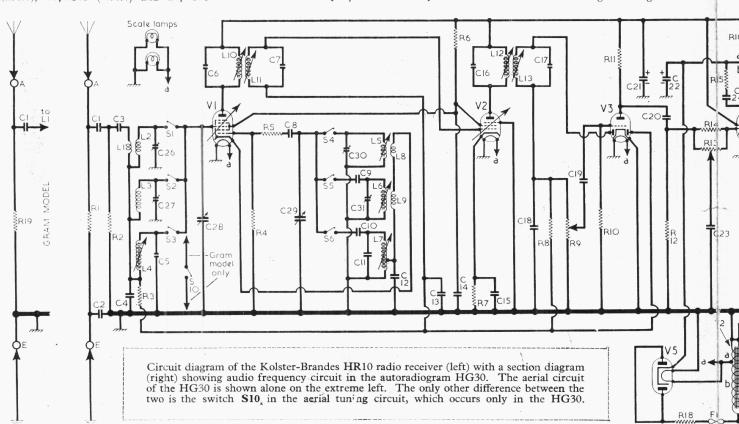
Audio frequency component in rectified output is developed across volume control R9, which acts as diode load, and is

passed via C19 to grid of triode section.

D.C. potential developed across R9 is fed back as bias to V1 and V2 giving automatic gain control. Second diode of V3 is connected to the A.G.C. line and prevents it from going positive. I.F. filtering by C18.

In the gram model the pick-up is connected across volume control R24 via S12, which closes in the gram position of the waveband switch control. \$10 closes and \$11 opens in this position to prevent radio break-through. At low level settings of the volume control C35, R25 and R26 give bass compensation. At higher set tings their effect is negligible. In the table receiver no provision is made for the connection of a gramophone pick-up, and all these switches are omitted. In the table receiver, resistance-capacitance coupling is effected by R11, C20 and R12, via the tone control circuit across R14, between V3 and tetrode output valve (V4, Brimar 6AQ5). Fixed tone correction by R15, C24 and by negative feed-back introduced by the omission of the normal bypass capacitor in the cathode circuit.

The variable tone control circuit R13, C23 introduces a variable degree of high-



COMPONENT VALUES AND LOCATIONS



The appearance of the K.-B. HR10. The HG30 ARG is shown overleaf.

note attenuation. Provision is made for the connection of a low-impedance external speaker across the output transformer secondary winding. Switch \$7 is provided to permit the internal speaker to be

In the gram version the coupling circuit between V3 and V4 is different. V3 anode is fed via R28, and V4 screen is fed from the same point. Coupling is by R29, C36 and R30, and the tone control circuit is modified, R31, C39 being shunted across R30. V4 cathode circuit is bypassed by C42.

H.T. current is supplied by I.H.C. full-wave rectifying valve (V5, Brimar 6X4). Smoothing by R16 and electrolytic capacitors C21, C22 in the table model, and by R33, C37 and C38 in the gram model.

(Continued column 1 overleaf)

			tions
R1	Anti-static shunt	$1 M\Omega$	G4
R2	Mod. hum shunt	$1 \mathrm{k}\Omega$	G4
R3	A.G.C. decoup	$100 \mathrm{k}\Omega$	G3
R4	V1 osc. C.G	$22\mathrm{k}\Omega$	F3
R5	Osc. stabilizer	47Ω	F3
R6	S.G. H.T. feed	$*16.5k\Omega$	E3
R7	V2 G.B	47Ω	E3
R8	A.G.C. decoup	$2 \cdot 2M\Omega$	E3
R9	Volume control	$500 \mathrm{k}\Omega$	E3
R10	V3 C.G	$10M\Omega$	E4
R11	V3 anode load	$470 \text{k}\Omega$	E4
R12	V4 C.G	$220 \mathrm{k}\Omega$	D3
R13	Tone control	$250 \mathrm{k}\Omega$	D3
R14	Part tone control	$470 \text{k}\Omega$	E3
R15	Tone corrector	$15 \mathrm{k}\Omega$	D4
R16	H.T. smoothing	820Ω	D4
R17	V4 G.B	$†280\Omega$	E4
R18	V5 surge limiter	$\pm 165\Omega$	F4
R19	Aerial shunt	$2 \cdot 2 k\Omega$	-
R20	I.F. stopper	$100 \mathrm{k}\Omega$	
R21	A.G.C. decoupling	$2 \cdot 2 \mathbf{M} \Omega$	
R22	P.U. shunt	$1.5M\Omega$	
R23	P.U. series	$2.2M\Omega$	
R24	Volume control	$500 \mathrm{k}\Omega$	-
R25) m	$4.7 k\Omega$	
R26	Tone compensators {	$10k\Omega$	
R27	V3 C.G	$10M\Omega$	
R28	H.T. feed	$1k\Omega$	
R29	V3 anode load	$470 \text{k}\Omega$	
R30	V4 C.G	$220 \mathrm{k}\Omega$	
R31	Tone control	$250 \mathrm{k}\Omega$	
R32	Tone corrector	$15k\Omega$	
R33	H.T. smoothing	$1k\Omega$	
R34	V4 G.B	240Ω	

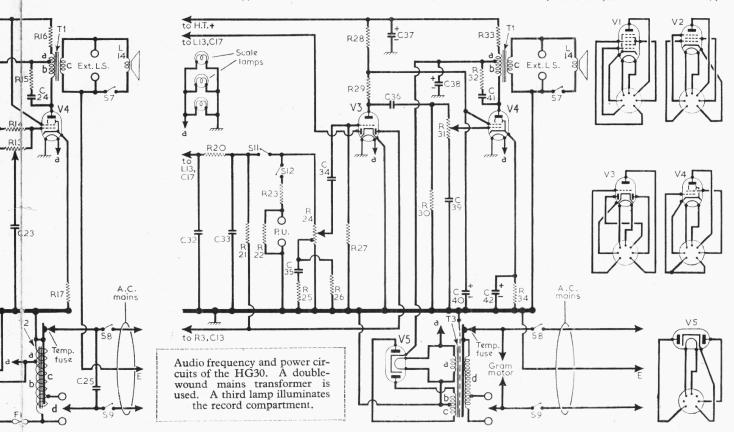
† Two 560Ω resistors in parallel ‡ Two 330 Ω resistors in parallel.

If the component numbers given in the accompanying tables are used when ordering replacement parts, dealers are advised to mention the fact on the order, as these numbers may differ from those used in the manufacturers' diagram.

Anti-static shunt MΩ G4 Mod, hum shunt $1 \text{K}\Omega$ G6 S4 Mod, hum shunt $1 \text{K}\Omega$ G3 S4 Mod, hum shunt $1 \text{K}\Omega$ G6 S4 Mod, hum shunt $1 \text{K}\Omega$ G3 S6 Mod, hum shunt $1 \text{K}\Omega$ G3 S6 Mod, hum shunt $1 \text{K}\Omega$ Mod	RESISTORSO	Salues (Loca- tions	.CO	CAPACITORS	Values	Loca- tions
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Mod. hum shunt A.G.C. decoup. V1 osc. C.G. Osc. stabilizer S.G. H. T. feed V2 G.B. A.G.C. decoup. Volume control V3 C.G. Tone control Part tone control Part tone control Part tone corrector H.T. smoothing V4 G.B. Surge limiter Aerial shunt L.F. stopper A.G.C. decoupling P.U. shunt P.U. series Volume control Tone compensators V3 C.G. H.T. feed V3 anode load V4 C.G. Tone control Tone control Tone control Tone control Tone corrector	1 kΩ 100kΩ 22kΩ 47Ω 47Ω 47Ω 47Ω 500kΩ 10MΩ 10MΩ 220kΩ 15kΩ 470kΩ 250kΩ 470kΩ 250kΩ 470kΩ 250kΩ 470kΩ 250kΩ 15kΩ 820Ω 22kΩ 10kΩ 2-2kΩ 10kΩ 2-2kΩ 10kΩ 1-5MΩ 2-2MΩ 500kΩ 10kΩ 1-5MΩ 10kΩ 10kΩ 10kΩ 10kΩ 10kΩ 10kΩ 10kΩ 10k	G4 G3 F3 F3 E3 E3 E3 E4 D3 D4 E4 F4 	C2 C3 C4 C5 C6 C7 C8 C9 C10 C11 C12 C13 C14 C16 C17 C18 C19 C21 C22 C23 C24 C25 C26 C26 C27 C28 C29 C30 C31 C30 C31 C32 C32 C31 C33 C34 C33 C34 C35 C36 C37 C37 C38 C37 C38 C31 C38 C31 C38 C31 C38 C31	Sisolators Sisolators Aerial coupling L.W. aerial trim Ist I.F. trans. Sit I.F. trans.	$\begin{array}{c} 0\text{-}0\text{-}1\mu\text{F} \\ 0\text{-}005\mu\text{F} \\ 0\text{-}005\mu\text{F} \\ 48\text{pF} \\ 88\text{pF} \\ 88\text{pF} \\ 88\text{pF} \\ 100\text{pF} \\ 410\text{pF} \\ 100\text{pF} \\ 0\text{-}02\mu\text{F} \\ 0\text{-}02\mu\text{F} \\ 0\text{-}02\mu\text{F} \\ 0\text{-}02\mu\text{F} \\ 330\text{pF} \\ 0\text{-}003\mu\text{F} \\ 32\mu\text{F} \\ 32\mu\text{F} \\ 32\mu\text{F} \\ 32\mu\text{F} \\ 40\text{pF} \\ 40\text{pF} \\ 40\text{pF} \\ 40\text{pF} \\ 40\text{pF} \\ 100\text{pF} \end{array}$	G4 G4 G4 G4 B1 B1 F4 F3 F3 E3 E3 C1 C1 C1 E3 D4 G4 A2 A2 F4 G4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				C34 C35	A.F. coupling Tone compensator	$0.01 \mu F \\ 0.05 \mu F$	
the component numbers given in the C42* V4 cath, by-pass 30µF —	0.560Ω resistors in paralogonal 0.330Ω resistors in paralogonal 0.330Ω	lel. allel.		C37* C38* C39 C40* C41	A.F. coupling H.T. smoothing { Part tone control H.T. decoupling Tone corrector	$20 \mu F$ $30 \mu F$ 800 p F $10 \mu F$ $0.003 \mu F$	

* Electrolytic. † Variable. ‡ Pre-set.

(" Other Components" table is overleaf.)



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| Compared to the content of the content

Underside view of the chassis. A diagram of the waveband switch unit **S1-S6** appears at the foot of col. 4.

The table below it gives the switch positions for the three control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.

\$7 is the screw-type speaker switch, mounted in a panel on the rear member of the chassis. When it is unscrewed (by turning it anti-clockwise a few times) the internal speaker speech coil is open-circuited, muting the speaker.

S8, S9 are the Q.M.B. mains switches, ganged with the variable tone control **R13.**

Scale Lamps.—These are two M.E.S.-type lamps with clear tubular bulbs. The makers' service manual quotes them as being Part No. 201/193, rated at 6 V, 0.2 A. Those in our sample were marked Ph. Gt. Brit. 6.5 V 0.3 A. They are mounted in rubber grommets which fit into recesses stamped in the scale backing plate. To remove the grommet from the lamp, stand the lamp up on its centre contact pip and press downwards on the grommet with both thumbs.

Fuse F1.—This is a standard 1¼in glass cartridge fuse mounted on the chassis deck behind the mains transformer. It is rated at 250 mA (colour coding brown).

Temperature Fuse.—This fuse actually consists of a special kind of solder, with a low temperature melting point. In practice the solder is used to hold a hairpin of springy phosphor-bronze strip to a bar of metal embedded in the windings

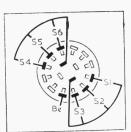


Diagram of the wave band switch unit, viewed from the rear of an inverted chassis. Below is the associated table.

Switch	L.W.	M.W.	S.W.
S1			С
82		С	
83	С		
84			С
85		С	
86	C		

of the mains transformer, so that if the latter overheats for any length of time, the heat conducted up to the joint melts the solder releasing the strip.

Normally when it "blows' it should be possible to replace it merely by melting the solder again with a clean soldering iron, holding the strip in place. In no circumstances must ordinary solder be added. If more solder is required, it should be obtained from the makers.

Record Unit.—The auto-changer is a Garrard RC75 3-speed unit taking 8 records unmixed. The pick-up is an Acos with a compromise type of sapphire needle that will suit 78, 45 and 33½ records. The pick-up is coded with a spot of white paint on the needle.

The makers of the radiogram state that where queries arise involving reference to the makers, dealers should approach the Garrard Engineering & Manufacturing Co., Ltd., direct concerning the changer, or Cosmocord, Ltd., concerning the pick-up.

External Speaker.—Two sockets are provided at the rear of the chassis for the connection of a low impedance (about $2-4\Omega$) external speaker. A switch $\bf 57$ mounted on the same terminal panel permits the internal speaker to be muted.

CIRCUIT ALIGNMENT

1.F. Stages.—Remove chassis from cabinet and place it in a convenient position on the bench. Connect signal generator output, via an $0.1\mu\mathrm{F}$ capacitor in each lead, to control grid (pin 7) of V1 and chassis. Switch receiver to M.W. and turn gang to minimum capacitance. Feed in a 422 kc/s (710.8 m) signal and adjust the cores of L13 (location reference E3), L12 (B2), L11 (B1) and L10 (F3) for maximum output, reducing the input as the circuits come into line to avoid A.G.C. action. Repeat these adjustments.

R.F. and Oscillator Stages.—As the tuning scale remains fixed in the cabinet when the chassis is withdrawn, reference should be made during the following alignment operations to the calibration marks on the scale backing plate. Check that with the gang at maximum capacitance the cursors coincide with the "D" calibration marks on the backing plate. Transfer signal generator leads, via a

standard dummy aerial, to A and E sockets.

M.W.—Switch receiver to M.W. and tune left-hand cursor to M.W. calibration mark near centre of backing plate. Feed in a 600 kc/s (500 m) signal and adjust the core of L6 (B2) for maximum output. Tune left-hand cursor to M.W. calibration mark at left-hand end of backing plate, feed in a 1,400 kc/s (214 m) signal and adjust C31 (A2) and C27 (A2) for maximum output. During the final adjustment of C27 rock the gang for optimum results. Repeat these adjustments until no further improvement results.

L.W.—Switch receiver to L.W., tune left-hand cursor to L.W. calibration mark, feed in a 225 kc/s (1,333 m) signal and adjust the cores of **L7** (B1) and **L4** (A2) for maximum output. Repeat these



The appearance of the autoradiogram HG30.

adjustments and then check the M.W. alignment, re-adjusting L6, C31 and C27, if necessary, as previously described.

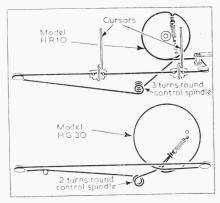
S.W.—Switch receiver to S.W., tune right-hand cursor to calibration mark "S" near centre of scale. Feed in a 6 Mc/s (50 m) signal and adjust the core of L5 (B2) for maximum output. Tune right-hand cursor to calibration mark "S" near right-hand end of backing plate. Feed in a 15 Mc/s (20 m) signal and adjust C30 (A2) and C26 (A2) for maximum output, rocking the gang while adjusting C26 for optimum results. Repeat these adjustments until no further improvement results.

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alloy and melts it, releasing the spring contact and breaking the mains input cir-

DRIVE CORD REPLACEMENT

Table Receiver .- Four feet of highgrade flax fishing line is required for a new drive cord, and this length leaves an ample margin for tying off. The cord should be run as shown in the upper drawing in the accompanying sketch,



Sketches showing the drive cord systems in the HR10 (above) and HG30 (below) models, as seen from the front, with the gang at maximum.

Approx. Values OTHER COMPONENTS (ohms) tions S.W. Aerial coup.... G3 $\begin{array}{c} L1 \\ L2 \\ L3 \\ L4 \\ L5 \\ L6 \\ L7 \\ L8 \\ L9 \\ L10 \\ L11 \\ L12 \\ L13 \\ L14 \end{array}$ G3Aerial tuning coils 18.0G4Oscillator tuning Osc. reaction coils \dots $\begin{array}{c} -0.0 \\ 20.0 \\ 20.0 \\ 20.0 \\ 20.0 \\ 2.2 \\ 1.5 \end{array}$ 1st I.F. trans. {Pri. Sec. B1 B1 2nd I.F. trans. ${PII. Sec.}$ Speech coil 160.0 C2T1O.P. trans. \\b $\begin{array}{c} \textbf{Mains trans.} \begin{cases} a \\ b \\ c \\ d \\ \end{array}$ $\substack{200\cdot0\\174\cdot0}$ T2B226.0 Mains trans. $\begin{cases} a & \dots \\ b & \dots \end{cases}$ 290.0 $T^{i}3$ Gram Model c ... d, total 290.0 49.0 Waveband switches G381-86Speaker switch ... Mains sw., g'd R13 87 88, 89 810- $\widetilde{\mathrm{D}}\widetilde{\mathrm{3}}$ Gram switches S12 F1 B2H.T. fuse, 250 mA

* Tapped at 0.6Ω from chassis.

Circuit Description-continued

Residual hum is neutralized in both models by passing the H.T. current through section a of T1 primary winding.

In the table model the anodes of V5 are strapped to form a half-wave rectifier and are fed from the 240 V tap on the mains auto-transformer T2. Another tapping on T2 feeds the heaters of all the valves, including V5. R18 and fuse F1 protect V5 from current surges and overloads respectively.

In the gram model a double-wound mains transformer is used and V5 operates as a full-wave rectifier with H.T. windings b and c on T3. Winding a on T3 feeds the heaters of all the valves, including V5.

In both models a temperature fuse is fitted to the mains transformer and consists of a spring contact, which is held by a low melting-point alloy to a copper strip embedded in the mains transformer, near the primary winding. One side of the mains is connected to the transformer primary through the temperature fuse, and if the transformer becomes overheated owing to a component breakdown, the copper strip conducts heat to the fusible

where the system is drawn as seen from the front with the gang at maximum capacitance. The maker's Part No. for a new drive cord assembly is 290/174.

Both ends of the cord are tied to the same end of the tension spring. makers' manual gives the number of turns round the control spindle as two, but in our sample there were three turns. The cord runs over a pulley at each end of the scale assembly, but behind the right-hand pulley in our sketch it runs round a smooth guide pin also, to bring it into line with the gang drum.

Radiogram.—Below the sketch of the drive for the table receiver, which was drawn from our sample chassis, is reproduced the maker's sketch of the drive system in the radiogram. This is viewed from the front also, with the gang at the maximum capacitance. About 5ft of cord is required.

It follows very much the same lines as

that in the table receiver, but the guide pin on the right is omitted and another is introduced on the left to bring the cord into line with the left-hand pulley. The maker's Part No. for a new drive cord assembly is 290/174/1.

DISMANTLING

Chassis.—Remove control Removing knobs (pull off) and unsolder leads from speech coil tags on speaker; remove two 2BA bolts (with shake-proof

washers) from front corners of chassis and withdraw chassis, disengaging it from the wood screws at the rear of the cabinet.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured on our receiver when it was operating from A.C. mains of 230 V. The receiver was switched to M.W. and tuned the high wavelength end of the band with the volume control at maximum, but there was no signal input.

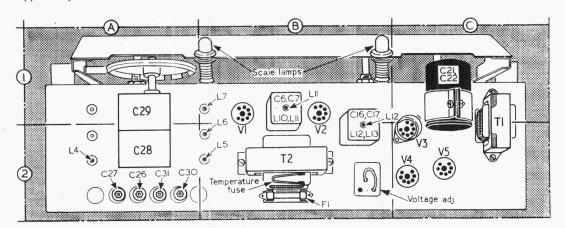
Voltage readings were measured with an Avo Electronic TestMeter, and as this instrument has a high internal resistance allowance should be made for the current drawn by other types of meter. Chassis was the negative connection in every case. The manufacturers' voltage figures for the gram model are about 10 per cent higher than the figures they quote for the table model.

Valve		Anode		Screen		Cath.
		. V	mA	v	mA	v
V1 6BE6 V2 6BA6		204 204	1·7 5·6	80 80	5·8 2·0	0.36
V3 6AT6 V4 6AQ5		60 215	0·33 29·0	204	4.2	9.2
V5 6X4		200†				220.0*

* Cathode current, 47mA. † A.C. reading.

GENERAL NOTES

Switches.-S1-S6 are the waveband switches, ganged in a single rotary unit beneath the chassis. The unit is indicated in our underside view of the chassis, and it is shown in detail in the diagram in col. 4, where it is drawn as seen when viewed from the rear of an inverted chassis.



Plan view of the chassis. The temperature fuse consists of a hairpin-shaped phos-phor-bronze strip soldered with special solder to the end of a heat-conducting bar sunk into the windings of the mains transformer.