# "TRADER" SERVICE SHEET ULTRA U506

885

H OUSED in a small plastic table cabinet, the Ultra U506 is a 4-valve (plus rectifier) 2-band receiver designed for A.C. or D.C. mains of 200-250 V, 40-100 c/s in the case of A.C. Miniature Mazda valves are used, with B8A bases. Slots in the chassis facilitate removal and replacement of waveband switch and volume control units.

Release date and original price: December 1947, £13 17s. 6d., reduced June 1948 to £13 15s. 4d. Purchase tax extra.

# CIRCUIT DESCRIPTION

Input from attached aerial via isolating capacitor C1 and coupling coils L2 (M.W.) and L3 (L.W.) to single-tuned circuits L4, C25 (M.W.) and L5, C25 (L.W.). An acceptor circuit L1, C2 shunts the aerial coupling coils and filters out signals at the intermediate frequency.

the intermediate frequency.

First valve (V1, Mazda 10C1) is a triode-hexode operating as frequency changer with internal coupling. Triode oscillator grid coils L6 (M.W.) and L7 (L.W.) are tuned by C26. Parallel trimming by C27 (M.W.) and C10, C28 (L.W.); series tracking by C11 (M.W.) and C12 (L.W.). Reaction coupling from anode, via C13, by coil L8 on M.W., and by the common impedance of C12 in grid and anode circuits on L.W.

and anode circuits on L.W.

Second valve (V2, Mazda 10F9) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned-transformer couplings C7, L9, L10,

C8 and C14, L11, L12, C15, in which the tuning capacitors are fixed and alignment adjustments are carried out by varying the positions of the iron-dust cores.

## Intermediate frequency 465 kc/s.

Diode second detector is part of double diode triode valve (V3, Mazda 10LD11), one diode of which is unused and wired to cathode. Audio frequency component in rectified output is developed across manual volume control R6, which is also the diode load resistor, and passed via A.F. coupling capacitor C17 and C.G. resistor R7 to grid of triode section, which operates as A.F. amplifier. I.F. filtering by C16, R5 in diode circuit.

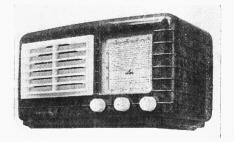
Resistance-capacitance coupling by R8, C18, R9 between V3 triode and beam tetrode output valve (V4, Mazda 10P13),

(Continued col. 1 overleaf)

## COMPONENTS AND VALUES

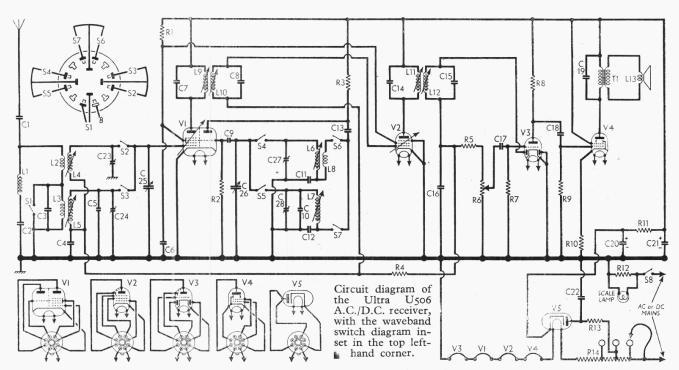
	RESISTORS	Values (ohms)	Loca- tions
R1	S.G.'s H.T. feed	27,000	<b>K</b> 5
R2	V1 osc. C.G	22,000	N5
R3	Osc. anode load	56,000	M5
R4	A.G.C. decoup	1,000,000	L4
$R_5$	I.F. stopper	100,000	K4
R6	Volume control	1,000,000	<b>K</b> 3
R7	V3 triode C.G	4,700,000	$H_4$
R8	V3 triode load	100,000	$H_5$
R9	V4 C.G. resistor	330,000	$H_5$
R.10	V4 G.B. resistor	270	G4
R11	H.T. smoothing	1,200	D2
R12	Scale lamp shunt	33	J4
R13	V5 surge limiter	100	F4
R14	Heater ballast	980†	E2

† Tapped at  $700\Omega + 200\Omega + 80\Omega$  from V5 heater.



$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CAPACITORS		Values (µF)	Loca- tions
C3			0.005	<b>A2</b>
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
C5			0.0001	M4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.05	M5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C5		0.00003	M4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		S.G.'s decoupling	0.05	K4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1st I.F. transformer	0.0001	B2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		∫ tuning \	0.0001	B2
C11		V1 osc, C.G	0.000075	N4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.000075	$M_5$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.00045	L4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C12	Osc. L.W. tracker	0.0002	$L_4$
C15	C13	Osc. anode coup	0.0001	N4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		2nd I.F. transformer	0.0001	C2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		∫ tuning \	0.00018	C2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		I.F. by-pass	0.00027	J4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		A.F. coupling capa-	0.01	J4
$ \begin{array}{c c} C20^* \\ C21^* \\ C21^* \\ C22 \\ C22 \\ C23^* \\ C23^* \\ C23^* \\ C23^* \\ C23^* \\ C23^* \\ C24^* \\ Aerial M.W. trim \\ C30^* \\ C25^+ \\ C26^* \\ C26^* \\ C26^* \\ C26^* \\ C30^* \\ C3$	C18	} citors }	0.01	$H_5$
C22     Mains R.F. by-pass     0-01     F4       C23‡     Aerial M.W. trim     0-00007     A1       C24‡     Aerial L.W. trim     0-00007     N4       C25†     Aerial tuning     0-000394     B1       C26†     Oscillator tuning     0-000394     B2       C27‡     Osc. M.W. trim     0-00007     N4			0.01	$\mathbf{H}3$
C22         Mains R.F. by-pass         0-01         F4           C23‡         Aerial M.W. trim         0-00007         A1           C24‡         Aerial L.W. trim         0-00007         N4           C25†         Aerial tuning         0-000394         B1           C26†         Oscillator tuning         0-000394         B2           C27‡         Osc. M.W. trim         0-00007         N4		H.T. smoothing	16.0	C1
C22     Mains R.F. by-pass     0-01     F4       C23‡     Aerial M.W. trim     0-00007     A1       C24‡     Aerial L.W. trim     0-00007     N4       C25†     Aerial tuning     0-000394     B1       C26†     Oscillator tuning     0-000394     B2       C27‡     Osc. M.W. trim     0-00007     N4		capacitors \		C1
C24‡     Aerial L.W. trim.     0.00007     N4       C25†     Aerial tuning     0.000394     B1       C26†     Oscillator tuning     0.000394     B2       C27‡     Osc. M.W. trim.     0.000007     N4		Mains R.F. by-pass	0.01	F4
C25† Aerial tuning 0·000394 B1 C26† Oscillator tuning 0·000394 B2 C27‡ Osc. M.W. trim 0·00007 N4	C23‡	Aerial M.W. trim	0.00007	A1
C26† Oscillator tuning 0·000394 B2 C27‡ Osc. M.W. trim 0·00007 N4		Aerial L.W. trim	0.00007	N4
C27‡ Osc. M.W. trim 0-00007 N4			0.000394	B1
		Oscillator tuning	0.000394	B2
[C28‡ Osc. L.W. trim, 0.00007 N4		Osc. M.W. trim	0.00007	N4
	[C28]	Osc. L.W. trim	0.00007	N4

\* Electrolytic. † Variable. ‡ Pre-set.



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OT	HER COMPONENTS;	Approx. Values (ohms)	Loca
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 T1 S1-S7	Acrial coupling coils  Acrial tuning coils  Oscillator tuning coils Osc. M.W. react  Ist I.F. trans. { Pri. Sec. Speech coil Output trans. { Pri. Sec. W/band switches Mains sw., g'd R6	7·5 47·0 175·0 3·0 20·0 3·5 7·5 1·75 7·0 7·0 7·0 6·0 3·0 30·0 0·75	A2 A1 N4 A1 N4 L4 L5 L4 B2 C2 C2 E1 H4 H4 N3 K3

# Circuit Description—continued

and fixed tone correction in tetrode anode circuit by C19.

When the receiver is operating from A.C. mains, H.T. current is supplied by half-wave rectifying valve (V5, Mazda U404), which behaves as a low resistance with D.C. mains. Smoothing by resistor R11 and electrolytic capacitors C20, C21.

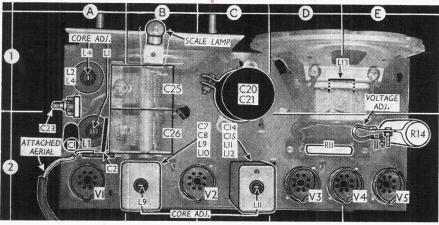
Valve heaters, together with scale lamp and adjustable ballast resistor R14, are connected in series across mains input. Mains R.F. filtering by C22.

# **VALVE ANALYSIS**

Valve voltages and currents given in the table below are those quoted by the manufacturers, and represent average "no signal" values to be expected in a receiver operating on A.C. mains of 230 V. Voltages were measured on the 400 V. scale of a model 7 Avometer, chassis being the negative connection.

Valve	Anode Voltage (V)	Anode Current (mA)		Screen Current (mA)
V1 10C1	186 Oscil	$\left\{\begin{array}{c} 1\cdot 3 \\ \text{lator} \\ 2\cdot 7 \end{array}\right\}$	50	4.4
V2 10F9 V3 10LD11	186	3.0 1.5	50	1.0
V4 10P13 V5 U404	179	26.0	186	6.3

† Cathode to chassis 244 V, D.C.



Plan view of the chassis, showing the aerial and I.F. transformer primary core adjustments. The attached aerial lead is soldered to a tag mounted on the frame of the gang unit.

## **DISMANTLING THE SET**

Removing Chassis.—Remove the three control knobs (recessed grub screws) and felt washers, from the front of the cabinet. From the underside of the cabinet remove the four machine screws securing the chassis and slide out the chassis and speaker as a single unit.

and single unit.

When replacing, do not omit to cover the heads of the chassis retaining screws and the control knob grub screws with a suitable insulation. ing compound.

## **GENERAL NOTES**

Switches.—\$1.\$7 are the waveband switches, ganged in a single two-position rotary unit beneath the chassis. This is indicated in our under-chassis view, and shown in detail in the diagram inset in the top left-hand corner of the circuit diagram overleaf, where it is drawn as seen from the rear of an inverted chassis.

\$1, \$2, \$4 and \$6 close on M.W. (knob anticlockwise) and open on L.W.; \$3, \$5 and \$7 close on L.W. and open on M.W.

\$cale Lamp.—This is an Osram M.E.S. type, with a small clear spherical bulb, rated at 3.5 V., 0.15 A. It is shunted by \$R12, and is energised by the combined heater and H.T.

energised by the combined heater and H.T.

Resistor R11.—This is the H.T. smoothing resistor, in a wire-wound enamelled unit rated at 1,200Ω, 5 W. It is mounted on a small panel on the chassis deck.

Chassis Divergencies.—In some chassis, C5 may be omitted, and C3 may be 0.00007μF. Also, C23, C24, C27 and C28 may be 0.00005μF.

Drive Cord Replacement.—This is very simple. The cord goes round the upper half of the drive drum and makes  $2\frac{1}{2}$  turns round the control spindle, still travelling in the same circular direction.

Access to the drum is obtained by removing the pointer (pull-off) and scale panel (slots under waveband switch and volume control fixing nuts) after unclipping scale lamp holder.

## CIRCUIT ALIGNMENT

The chassis must be removed from the cabinet before commencing operations.

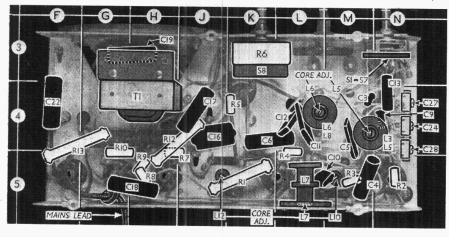
1.F. Stages.—Connect signal generator, via an 0.1 μF isolating capacitor in each lead, to control grid (pin 6) of V1 and chassis, switch set to M.W., turn gang and volume control to maximum, and feed in a 465 kc/s (645.16 m) signal. Adjust the cores of L12, L11, L10 and L9 (location references J5, C2, M5, B2) for maximum output, progressively attenuating the input signal as the circuits are aligned to minimize A.G.C. action. Finally, disconnect "live" signal generator lead from V1.

R.F. and Oscillator Stages.-With the gang at maximum capacitance the pointer should be horizontal. It may be adjusted in position by rotating it on the gang spindle. Transfer "live" signal generator lead to attached aerial connecting tag (A2), via a suitable dummy aerial.

I.F. Filter.—With the set switched to M.W., feed in a 465 kc/s signal, and adjust the core of L1 (A2) for minimum output.

M.W.—With the set switched to M.W., tune to 230 m on scale, feed in a 230 m (1,304 kc/s) signal, and adjust C27 (N4) and C23 (A1) for maximum output. Tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and adjust the cores of L6 (L4) and L4 (A1) for maximum output. Repeat these operations until no improvement results.

L.W.—Switch set to L.W., tune to 1,000 m on scale, feed in a 1,000 m (300 ke/s) signal, and adjust **C28** and **C24** (N4) for maximum output. Tune to 2,000 m on scale, feed in a 2,000 m (150 kc/s) signal, and adjust the cores of **L7** (L5) and L5 (M4) for maximum output. Repeat these operations until no improvement results.



Under-chassis view. The waveband switch unit S1-S7 is shown in detail in the diagram inset in the circuit diagram overleaf. The oscillator and I.F. transformer secondary core adjustments are indicated.